SUBWOOFER WITH CASCaded LINEAR ARRAY OF DRIVERS

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Appl. No.: 10/649,040

Filed: Aug. 27, 2003

ABSTRACT

A single folded, expanding horn loudspeaker reproduces low frequency audible sound at high power output levels. A compact enclosure houses a plurality of identical transducers, characterized by small vibrational surface areas. The throats for each transducer into the horn are acoustically differentially spaced from the mouth of the horn. Transducer drive circuitry adjusts a drive signal for the transducers to compensate for the different impedance and propagation time to the horn mouth at each throat.
From Audio Freq. Source

Band Pass
Filtering and Frequency Shading

Time Delay

Dynamic Phase Adjustment as a $F(t)$

To Amplifier

Fig. 8
SUBWOOFER WITH CASCaded LINEAR ARRAY OF DRivers

BACKGROUND OF THE INVENTION

[0001] 1. Technical Field

[0002] The invention relates to an electro-acoustical device and, more particularly, to a folded horn loudspeaker for reproducing low frequency audible sound at high output levels from electric-acoustic transducers having relatively small diaphragms.

[0003] 2. Description of the Problem:

[0004] The reproduction of low frequency audible sound, with high fidelity and at high intensity levels, poses a number of challenges. To do so from a small, energy efficient package, portable enough to be moved and suitable for open air use is especially difficult. Generally, high output, high efficiency, low frequency loudspeakers have been built around a horn. A horn is in effect an acoustic transformer, allowing the designer to obtain the output performance of a driving unit having a large area diaphragm from a unit having a smaller area diaphragm while minimizing cone/diaphragm resonance issues that exist with direct radiator devices. Increasing the effective diaphragm area renders radiation impedance increasingly resistive with the result that increasing power is radiated at the desired low frequencies. However, increasing acoustic power output from most horn designs has required increasing diaphragm piston travel in order to move the required volume velocity of air. Piston travel becomes an important limiting factor relating to the amount of power that can be delivered to the horn.

[0005] Another limitation on the total energy input that can be introduced to a horn has been the limited scalability of horns. Though examples of multiple driver horns are known, typically only a single driving unit for a given frequency range has been provided. One example of a multiple driver horn (U.S. Pat. No. 5,898,138) positions a pair of low frequency transducers having throats located equidistant from the horn’s mouth. While effective such an arrangement is still not readily scalable.

SUMMARY OF THE INVENTION

[0006] According to the invention there is provided a folded, expanding horn loudspeaker having a selectable plurality of acoustic drivers for a given frequency range. The loudspeaker unit provides a compact enclosure defining the folded, expanding horn and housing the acoustic drivers. A scalable number of identical acoustic drivers is provided, each having a relatively small cone or diaphragm, and each being located in a scaled back chambers (i.e. a closed box baffle). The acoustic drivers radiate into volumetrically identical high pressure chambers located in front of the drivers. The acoustic drivers are preferably positioned with respect to one another in a linear array and may vary in number from 2 to 12. Each high pressure front chamber is coupled to a summing throat for the horn by an extended port which operates as a air pressure or air volume velocity step up transformer. The outlets of the ports are acoustically spaced from one another and differentially spaced from the mouth of the horn. Transducer drive circuitry applies drive signals to the acoustic transducers derived from a common source. The signals to the respective acoustic transducers are delayed to reflect the distance of the throats for the respective acoustic transducers from the mouth of the horn. The source signal is also as filtered and phase adjusted as required for clear reproduction of the sound.

[0007] Additional effects, features and advantages will be apparent in the written description that follows.

BRIEF DESCRIPTION OF THE DRAWINGS

[0008] The novel features believed characteristic of the invention are set forth in the appended claims. The invention itself however, as well as a preferred mode of use, further objects and advantages thereof, will best be understood by reference to the following detailed description of an illustrative embodiment when read in conjunction with the accompanying drawings, wherein:

[0009] FIG. 1 is a perspective view of a loudspeaker enclosure;

[0010] FIG. 2 is a perspective view of the loudspeaker horn.

[0011] FIG. 3 is a cross sectional view of the loudspeaker enclosure of FIG. 1 taken along section line 3–3.

[0012] FIG. 4 is a cross sectional view of the loudspeaker enclosure of FIG. 1 taken along section line 4–4.

[0013] FIG. 5 is a cross section of a transducer housing taken along section line 5–5 in FIG. 3.

[0014] FIG. 6 is a rear elevation of the enclosure of FIG. 1 with the back panel of the enclosure removed.

[0015] FIG. 7 is a block diagram schematic of drive circuitry for the loudspeaker.

[0016] FIG. 8 is a block diagram schematic of the operation of the circuitry of FIG. 7.

[0017] FIG. 9 is a side elevation of a high pressure chamber exited by paired drivers.

DETAILED DESCRIPTION OF THE INVENTION

[0018] Referring now to the figures and in particular to FIG. 1 there is illustrated a loudspeaker system 10 for use as a high output, transportable unit. Loudspeaker system 10 comprises a right trapezoid enclosure or cabinet 11 which houses sound radiators and a folded waveguide or horn having a mouth 12 in front wall 14. Mouth 12 directs sound radiated from loudspeaker system 10 forward from the unit. Enclosure 11 is constructed from front wall 14, a back wall, a first side wall 16, a second side wall (described below), a cover 18 and a base 20. The bases and walls are conventionally made of plywood or some other material which does not readily absorb sound.

[0019] Referring to FIG. 2, enclosure 11 is presented in phantom at a reverse angle from the view of FIG. 1. Folded horn 22 is optimized for low frequency use and is constructed from flat sides and incorporates a flair, as is conventional. Folded horn 22 is disposed along side walls 16, 17 and the back wall 15 of enclosure 11 which form portions of the horns walls. Folded horn 22 expands cross-sectionally along its entire length from a base end 161, adjacent which the horn has its minimum cross-sectional area, to end 163 where the mouth of the horn is located. Folded horn 22
expands initially both vertically and horizontally, but eventually only in the horizontal dimension. A summing throat 61 is disposed along side 17 which expands in both the vertical and horizontal directions to a fold 151, where it matches with a first backside section 121. Backside section 121 continues to expand in two mutually perpendicular directions up to a second backside section 123. Section 123 is characterized by horn 22 having a constant vertical dimension, however expansion continues in the horizontal dimension at a rate consistent with the horn's flare constant. Vertical expansion is stopped in second backside section 123 not for functional reasons, but for external packaging reasons. Section 123 meets the final horn section 125, which continues to expand in the horizontal dimension, along fold 153. Loudspeakers are nested in the pocket 200 formed by and partially enclosed by the exterior faces of folder horn 22.

FIG. 3 is a cross sectional view of enclosure 11 taken along section line 3-3 in FIG. 1. Four walls form the perimeter, exterior sides of enclosure 11 including front wall 14, first side wall 16, back wall 15 and a second side wall 17. The perimeter formed by these walls is broken only by mouth 12 which provides a radiating outlet from the waveguide, i.e. folded, expanding horn 22. Folded horn 22 comprises four major sections and two bends or folds and, as described above, a rectangular cross sectional shape. A horn flare is provided by increasing the area of the section with distance through the horn 22. Initially, the cross-sectional dimensions of folded horn 22 increase in both the vertical and horizontal dimensions, but eventually only in the horizontal. Folded horn 22 includes a summing throat 61 into which four ports or extended throats 58, 60, 62 and 64 are directed. Folded horn 22 expands both vertically and horizontally for the entire length of summing throat 61. Folded horn 22 is divided into two sections 121 and 123 along back wall 15 of enclosure 11. Section 121 continues the two dimensional cross sectional expansion of fold horn 22 from summing throat 61. Section 123 expands only horizontally. Running from section 123 to mouth 12 is the final horn section 125, which also expands only in the horizontal direction.

Four acoustic drivers or transducers 26, 28, 30 and 32 are positioned in enclosure 11 (the latitudinal positions of which are illustrated in phantom) and oriented to direct sound downwardly into four high pressure (or preload) chambers 34, 36, 38 and 40 located directly above base 20. The upper surface of base 20 forms the bottom surfaces of high pressure chambers 34, 36, 38 and 40 which are aligned with one another. Acoustically absorbent pads 42, 44, 46 and 48 are positioned on the upper surface of bottom board 20 within each of chambers 34, 36, 38 and 40 to deaden resonance. Pads 42, 44, 46, 48 correspond to and are vertically aligned with acoustic drivers 26, 28, 30, 32, respectively. High pressure chambers 34, 36, 38 and 40 have acoustic outlet ports formed by extended throats 58, 60, 62 and 64, respectively. Extended throats 58, 60, 62 and 64 direct energy into summing throat 61. The outlets from extended throats 58, 60, 62 and 64 act as diaphragms aligned along one side of the summing throat 61 of folded throat 22. These outlets are at different distances from mouth 12 and, as a consequence, see different output impedances and have different propagation times for the sound energy they emit to mouth 12. The phase and frequency response of horn 22 will differ with respect to extended throats 58, 60, 62 and 64, sometimes in ways difficult to predict in advance for particular horn parameters and thus empirical evaluation may be required to determine the best dynamic phase adjustments, frequency band widths and roll offs to be used with the drive signal for each of the acoustic drivers 26, 28, 30 and 32. High pressure chambers 34, 36, 38, 40 each have the same volume as one another and the throats 58, 60, 62 and 64 have the same cross sectional areas as one another.

Each extended throat 58, 60, 62 and 64 has a cross sectional area which is at least 20% of the area of diaphragm for the corresponding acoustic drivers 26, 28, 30 and 32. High pressure chambers 34, 36, 38, 40 absorb much more power per unit of movement of the diaphragm allowing much larger driver motors 226, 228, 230 and 232 to be employed than in prior art devices. These motors may be two to three times as powerful as is conventional. For example, a 6-inch woofer may be driven by a watt drive coil. For maximum power input diaphragm 326, 328, 330 and 332 may be pushed at velocities up to the point of destructive turbulence in the extended throats 58, 60, 62 and 64.

The high pressure chambers, back chambers, extended throat and summing throat 61 are formed in part by vertical interior walls supported from base 20. Vertical interior wall 33 provides a portion of one side of folded horn 22 adjacent mouth 12 opposite the side provided by first exterior side wall 16. Vertical interior wall 33 and side wall 16 diverge from one another toward mouth 12 to provide an expanding cross-sectional area for horn 22. Vertical side wall 33 also provides an interior wall for each of extended throat 58, 60, 62 and 64 and for front chambers 34, 36, 38 and 40. The horizontal perimeter of preload or high pressure chamber 34 is completed by vertical walls 25, 41 and 70. The horizontal perimeter of high pressure chamber 36 is completed by vertical walls 27, 41 and 72. The horizontal perimeter of high pressure chamber 38 is completed by vertical walls 29, 41 and 74. The horizontal perimeter of high pressure chamber 40 is completed by vertical walls 31, 41 and 76. Wall 41 is broken in three places by outlets from throat extension guides 61, 62 and 64. The horizontal perimeters of high pressure chambers 34, 36, 38, 40 are broken by throats 50, 52, 54, 56. The horizontal perimeter of throat extension section 58 is completed by vertical walls 14 and 70. The horizontal perimeter of throat extension section 60 is completed by vertical walls 25 and 72. The horizontal perimeter of throat extension section 62 is completed by vertical walls 27 and 74. The horizontal perimeter of throat extension section 64 is completed by vertical walls 29 and 76. Vertical walls 33, 50, 72, 74 and 76 all continue upwardly to provide perimeter elements of substantially sealed back chambers (or closed-box baffles) for acoustic drivers 26, 28, 30 and 32.
[0024] Referring to FIG. 4, which is a cross-sectional view taken along section line 4-4 in FIGS. 1 and 2 and to FIG. 5, which is view taken into enclosure 11 along section line 5-5 in FIG. 4, the positioning of acoustic drivers 26, 28, 30, 32 over high pressure chambers 34, 36, 38 and 40 is illustrated. Acoustic drivers 26, 28, 30, 32 are housed in sealed back chambers 80, 82, 84 and 86, respectively. The term “sealed” as used here has its conventional meaning in the acoustical arts to mean that the back chambers have no acoustic outlet port. The only acoustic opening from sealed back chambers 80, 82, 84 and 86 are those directly in front of the diaphragms of acoustic drivers 26, 28, 30 and 32. Back chambers 80, 82, 84 and 86 do slowly exchange air with their ambient environment, as is conventional.

[0025] In FIG. 5 the position of extended 60 in front of wall 72 illustrates the interface of a representative high pressure chamber 36 to its extended throat 60 and further into summing throat 61. Because the upper cover section 91 is not horizontal, but slants upwardly from the base of summing throat 61 toward the back wall 15, the outlet from extended throats into summing throat 61 differs for each extended throat. Extended throat 60 includes some freeboard on wall 41 above the outlet and below upper cover section 91. As illustrated in FIG. 6 and described with reference to the figure below, the amount of freeboard for each port will differ. Acoustic driver 28 rests on a support plane 93. Sealed back chamber 82, like the remaining back chambers, is closed on one side by a planer wall 95.

[0026] Referring now to FIG. 6, which is an end view of enclosure 11 with back wall 15 removed, the interior of folded horn 22 is illustrated in greater detail, particularly the summing throat 61. Summing throat 61 is formed by portions of side wall 17, cover 91, base 18 and wall 41. Summing throat 61 collects sound output from the four throat extension sections 58, 60, 62, 64, the radiating outlets of which are visible along a side of summing section 61 defined by vertical wall 41. The surfaces forming summing throat 61 diverge from one another moving toward the back wall 15 from the base of the horn along front wall 14. The divergence of the upper and lower surfaces of folded horn 22 is provided in the upward slant of board 97. While the output port from extended throat 58 has a vertical extent substantially equal to the local height of summing throat 61, the outlets of downstream extended throats 60, 62 and 64, which are all of the same height, will have increasing amounts of freeboard.

[0027] Any given horn has differing horizontal and polar frequency responses. And while a horn may operate well at certain frequencies its performance can degrade markedly at other frequencies. These changes in performance are highly dependent on the length of the horn. While each of transducers 26, 28, 30, 32 is coupled to the folded horn by an identical high pressure chamber and extended throat, the extended throats in 56, 60, 62 and 64 are coupled to summing junction 61 at points which are differently spaced from the mouth 12. In other words, horn 22 will have different performance characteristics for each transducer including, different optimal frequency operating range. Accordingly, each driver circuit differentially treats the signal applied to each transducer.

[0028] Producing sound of maximum intensity from loudspeaker system 10 requires that acoustic pressure waves from the outlets of extended throats be synchronized at the points where they merge. Due to the different distances sound travels to reach mouth 12 from the outlets from extended throats 58, 60, 62 and 64, the drive signal applied to transducers 26, 28, 30, 32 is time differentiated so that the sound waves constructively reinforce one another in summing section 61 rather than cancel or interfere with one another. While the same signal is the genesis of the signal used to drive each of the four transducers 26, 28, 30, 32, this source signal must be processed differently before application to the respective transducers’ voice coils to assure good phase matching at the mouth 12 and a good match of output from the extended throats 58, 60, 62 and 64 to the frequency response characteristic of folded horn 22 for a given outlet port from one of extended throats 58, 60, 62 and 64. The signal for the transducer associated with the throat radiating end removed by the greatest distance from mouth 12 is delayed least, while the signal driving the transducer associated with the throat radiating end closest to mouth 12 is delayed by the greatest period. Differences in impedance matching of the extended throat for each driver to summing section 61 require some band pass filtering and shading of the source signal for optimal system performance. The source signal may require dynamic phase adjustment (i.e. adjustment of the signal phase as a function of frequency) of the source signal due to the frequency response characteristics of the horn which vary with frequency at each extended throat outlet port.

[0029] Referring to FIGS. 7 and 8, a common source 711 of audio frequency signals is applied to four inputs of a digital signal processor (DSP) 709 which differentially processes the signals to accommodate the relative positions of acoustical drivers 26, 28, 30, 32. DSP 709 provides the four differentiated outputs on each of four channels 713, 715, 717, 719 to four amplifiers 701, 703, 705 and 707 associated with acoustical drivers 26, 28, 30, 32. In general, the input signal is processed in the same general way for all four channels, with only the parameters applied by the processing steps changing. For each channel, the signal is fed through a band pass filter 801 which passes frequency ranges best handled by a particular horn/driver configuration. Typically, the broadest band of frequencies is applied to the acoustic driver couple to the summing junction 61 at the furthest point from mouth 12. The roll off of the signal range applied to a driver may also be adjusted. Next, the filtered signal is applied to a time delay 803 which synchronizes the signals based on the differing distances of the speakers from the horn mouth. Lastly, the filtered, delayed signal for a channel is applied to a dynamic phase adjustment module 805 which adjusts the phase of the signal as a function of frequency. The specific parameters used will change along with changes in horn dimensions and the number of transducers used.

[0030] FIG. 9 illustrates an alternative embodiment of the invention whereas two acoustic drivers 930A and 930B are coupled to a common high pressure chamber 900. Sound is coupled from compression chamber 900 to a horn 922 by an extended throat 902 which has a cross sectional area which is a fraction of the area of the diaphragms of acoustic drivers 930A-B. Extended throat 902 operates as a kind of pneumatic amplifier greatly accelerating air velocity. Still other arrangements of transducers and horn types will now occur to those skilled in the art.
[0031] The invention provides high acoustic output power for low frequency sound from a minimally sized, portable cabinet, suitable for use at outdoor, temporary venues. The package is well suited for bass line reproduction required for rock music reproduction.

[0032] While the invention is shown in only one of its forms, it is not thus limited but is susceptible to various changes and modifications without departing from the spirit and scope of the invention.

What is claimed is:
1. A loudspeaker comprising:
   an enclosure including a folded horn having a mouth;
   a plurality of acoustic transducers housed in the enclosure;
   a throat associated with each transducer for coupling the output of the transducer into the folded horn; and
   throat outlets being differentially spaced from the mouth.
2. A loudspeaker as set forth in claim 1, further comprising:
   a source of an acoustic range signal; and
   transducer drive signal processing circuitry having an individual channel for each of the audio transducers, the individual channels each being coupled to receive the acoustic range signal and each channel including a time delay element for delaying a signal in a channel as a function of the distance of the throat for the audio transducer associated with the channel from the mouth of the folded horn.
3. A loudspeaker as set forth in claim 2, further comprising:
   a plurality of high pressure chambers, at least one acoustic transducer being positioned to direct sound energy into each high pressure chamber, each high pressure chamber further having an elongated port to the folded horn providing a throat for the high pressure chamber.
4. A loudspeaker as set forth in claim 3, each channel of the transducer drive signal processing circuitry further comprising:
   a band pass filter receiving the acoustic range signal and producing a filtered signal therefrom;
   the time delay element receiving filtered signal and producing a delayed, filtered signal; and
   a dynamic phase adjustment element receiving the delayed, filtered signal and adjusting the phase of the signal as a function of frequency to produce a drive signal for an acoustic transducer.
5. A loudspeaker as set forth in claim 4, further comprising:
   a summing section of the folded horn into which each throat is coupled.
6. A loudspeaker as set forth in claim 5, further comprising:
   the acoustic transducers having a small vibrational surface area relative to the predominant range of frequencies to be reproduced; and
   a plurality of sealed back chambers, one sealed back chamber housing each acoustic transducer.
7. A loudspeaker as set forth in claim 6, further comprising:
   the audio transducers being positioned with respect to one another in a linear array, one to each high pressure chamber.
8. A loudspeaker as set forth in claim 6, further comprising:
   a plurality of acoustic transducers coupled to each high pressure chamber.
9. A loudspeaker as set forth in claim 4, wherein the band pass filters, delay elements and dynamic phase adjustment elements are realized in a digital signal processor.
10. Apparatus comprising:
    a plurality of acoustic transducers including at least two substantially identical acoustic transducers;
    a plurality of high pressure chambers with an acoustic transducer associated with each high pressure chamber, including two high pressure chambers of substantially the same volume into which the output of one each of the two substantially identical acoustic transducers is directed;
    an extended acoustic port from each high pressure chamber; and
    a horn having a summing section connected to a radiating end of each extended acoustic port and a mouth, the radiating ends of the extended acoustic ports associated with the two high pressure chambers of substantially the same volume being differentially spaced in terms of acoustic propagation time from the mouth.
11. Apparatus as claimed in claim 10, further comprising:
    means for coordinating operation of the two substantially identical acoustic transducers so that the pressure waves from the radiating ends of the acoustic ports reinforce one another.
12. Apparatus as claimed in claim 11, wherein the acoustic transducers are aligned side by side.
13. Apparatus as claimed in claim 11, wherein the acoustic transducers are housed in sealed back chambers.
14. Apparatus as claimed in claim 11, the means for coordinating further comprising drive circuitry for the substantially identical acoustic transducers including delay means for synchronizing the pressure waves upon their meeting in the summing section.
15. Apparatus as claimed in claim 14, the drive circuitry including a pass band filter associated with each of the substantially identical transducers and a dynamic phase adjustment element for each of the substantially identical acoustic transducers.

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